



## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

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<p>(54) Title: AROMATIC ALKYLATION WITH ALPHA-OLEFIN DIMER</p> <p>(57) Abstract</p> <p>A process is disclosed for the production of novel monoalkylbenzenes or substituted benzenes by aromatics alkylation wherein the alkylation catalyst is an acidic shape selective metallosilicate catalyst and the alkylating agent is the olefinic dimer by-product of the oligomerization of alpha-olefins in contact with reduced valence state solid chromium oxide catalyst on a porous support. The alkylated benzenes produced comprise those mono-alkylbenzenes wherein the alkyl group contains 12 to 28 carbon atoms and have high viscosity index, low pour point and low viscosity. They have a low degree of residual olefinic unsaturation and are useful as additives to thermally and oxidatively stabilize lubricant materials. The process comprises reacting benzene or substituted benzene with C<sub>6</sub>-C<sub>14</sub> alpha-olefin olefinic dimer having a branch ratio of less than 0.19, or mixture of the dimers, in contact with acidic shape selective zeolite catalyst having large pore size.</p>		

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AROMATIC ALKYLATION WITH ALPHA-OLEFIN DIMER

5 This invention relates to a process for the preparation of synthetic oils useful as lubricants, lubricant additives and insulating fluids. More particularly, the invention relates to a process for the monoalkylation of aromatic hydrocarbons with novel olefins obtained from the oligomerization of  $C_6-C_{20}$  alpha-olefins where the alkylating agent is the alpha-olefin oligomerization dimer.

10 It has been well established in the prior art that hydrocarbon oils possessing superior properties in applications such as low viscosity lubricants, insulating fluids for electrical transformers, additives for lubricants, and the like can be prepared by alkylation of aromatic compounds using higher molecular weight olefins and olefinic oligomers.

15 U.S. patent 4,238,343 to Pellegrini, Jr. discloses a synthetic oil composition useful as an insulating fluid in electrical apparatus comprising the mono or di-alkylation product from the alkylation of aromatics with oligomers containing at least 30 and up to 60 carbon atoms. The oligomers are prepared by Lewis acid catalysis by methods well known in the art. The  
20 alkylation reaction is conducted using conventional liquid Lewis acid catalyst and the degree of substitution is controlled by the aromatic to olefin mole ratio. Dimers are separated from oligomers and not included in the alkylation reaction.

25 U. S. patent 4,604,491 to Dressler et al. discloses a synthetic oil composition for functional fluids such as lubricants, heat transfer fluids, vacuum pump oils, etc. The compositions comprise mono and polyalkylated naphthalenes prepared by the alkylation of naphthalene with alpha-olefins in  
30 contact with high silica zeolites. The alkyl substituent on naphthalene contains between 12 and 26 carbon atoms.

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U.S. patent 4,714,794 to Yoshida et al. discloses a synthetic oil composition comprising monoalkylated naphthalene obtained by alkylation of naphthalene with alkyl halide, alcohol or a straight chain mono-olefin having six to twenty four carbon atoms. The mole ratio of alpha to beta substitution on naphthalene is at least 1.0. The products exhibit high oxidation stability.

Recently, novel lubricant compositions (referred to herein as HVI-PAO) comprising polyalpha-olefins and methods for their preparation employing as catalyst reduced chromium on a silica support have been disclosed in U.S. patents 4,827,064 and 4,827,073. The process comprises contacting C<sub>6</sub>-C<sub>20</sub> 1-alkene feedstock with reduced valence state chromium oxide catalyst on porous silica support under oligomerizing conditions in an oligomerization zone whereby high viscosity, high viscosity index (VI) liquid hydrocarbon lubricant is produced having branch ratios less than 0.19 and pour point below -15°C. The process is distinctive in that little isomerization of the olefinic bond occurs compared to known oligomerization methods to produce polyalpha-olefins using Lewis acid catalyst. Lubricants produced by the process cover the full range of lubricant viscosities and exhibit a remarkably high viscosity index (VI) and low pour point even at high viscosity. The as-synthesized HVI-PAO oligomer has a preponderance of terminal olefinic unsaturation.

In the preparation of the novel HVI-PAO lubricant, alpha-olefin dimer containing olefinic unsaturation can be separated from the oligomerization reaction. The composition of the dimer mixture conforms to the unique specificity of the oligomerization reaction in that little double bond isomerization is found and shows a low branch ratio.

It has been found that novel monoalkylbenzenes or substituted benzenes can be produced by an aromatics alkylation

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process wherein the alkylation catalyst used is an acidic shape selective metallosilicate catalyst and the alkylating agent is the olefinic dimer by-product of the oligomerization of alpha-olefins in contact with reduced valence state solid chromium oxide catalyst on a porous support. The olefinic dimer is the by-product of an oligomerization process notable for the very low degree of double bond isomerization occurring during the reaction such that the oligomer hydrocarbons and dimer by-products produced show branch ratios below 0.19. The alkylated benzenes produced comprise those mono-alkylbenzenes wherein the alkyl group contains 12 to 28 carbon atoms.

It has been further found that the monoalkylbenzenes of the present invention have high viscosity indices, low pour point and low viscosity. They have a low degree of residual olefinic unsaturation and are useful as additives to thermally and oxidatively stabilize lubricant materials. They are, of themselves, useful as low viscosity lubricants.

More particularly, a process is disclosed for the production of aromatic hydrocarbon synthetic oil comprising the steps of:

contacting  $C_6-C_{14}$  alpha olefin with a supported solid reduced metal oxide catalyst under oligomerization conditions at a temperature of 90 to 250°C, the metal oxide comprising a lower valence form of at least one Group VIB metal to produce lubricant range hydrocarbon product oligomers having a branch ratio of from 0.10 to 0.19 and a viscosity index of at least 130;

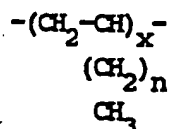
separating the oligomers and recovering  $C_{12}-C_{28}$  olefinic dimer by-product by distillation; and

reacting benzene or substituted benzene with the dimer, or mixture of the dimer, in contact with acidic shape selective metallosilicate catalyst under alkylating conditions whereby mono-alkylbenzenes containing  $C_{12}-C_{28}$  alkyl group are produced.

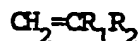
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In the present invention aromatic hydrocarbons are alkylated with unique olefin dimers produced as by-product in the oligomerization of 1-alkenes in contact with reduced chromium oxide on silica support. A characteristic of the novel oligomerization reaction from which the by-product dimers used as alkylating agent in the present invention are produced is the production of mixtures of dialkyl vinylidenic and 1,2 dialkyl or trialkyl mono-olefin oligomers (referred to herein as HVI-PAO oligomers), as determined by infra-red and nuclear magnetic resonance (NMR) analysis.

In general, the HVI-PAO oligomers have the following regular head-to-tail structure where  $n$  is preferably 0 to 17, terminating in olefinic unsaturation:



with some head-to-head connections. The HVI-PAO process produces a surprisingly simpler and useful dimer compared to the dimer produced by 1-alkene oligomerization with  $\text{BF}_3$  or  $\text{AlCl}_3$  as commercially practiced. Typically, in the present invention it has been found that a significant proportion of unhydrogenated dimerized 1-alkene, or alpha-olefin, has a vinylidenyl structure as follows:



where  $\text{R}_1$  and  $\text{R}_2$  are alkyl groups representing the residue from the head-to-tail addition of 1-alkene molecules. For example, the by-product dimer from 1-decene oligomerization according to the HVI-PAO process, which can be used as alkylating olefin in the present invention, has been found to contain three major components, as determined by GC. Based on  $^{13}\text{C}$  NMR analysis, the unhydrogenated components were found to be 8-eicosene, 9-eicosene, 2-octyldodecene and 9-methyl-8 or 9-methyl-9-nonadecene.

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Olefins suitable for use as starting material in the preparation of olefinic HVI-PAO oligomers and the by-product dimer used as starting material in the present invention include those olefins containing from 6 to 14 carbon atoms such as 1-hexene, 1-octene, 1-decene, 1-dodecene and 1-tetradecene and branched chain isomers such as 4-methyl-1-pentene. Also suitable for use are olefin-containing refinery feedstocks or effluents. However, the olefins used in this invention are preferably alpha olefinic as for example 1-octene to 1-dodecene and more preferably 1-decene, or mixtures of such olefins.

HVI-PAO oligomers of alpha-olefins used in this invention have a low branch ratio of less than 0.19 and superior lubricating properties compared to the alpha-olefin oligomers with a high branch ratio, as produced in all known commercial methods.

This class of unsaturated HVI-PAO alpha-olefin oligomers are prepared by oligomerization reactions in which a major proportion of the double bonds of the alpha-olefins are not isomerized. These reactions include alpha-olefin oligomerization by supported metal oxide catalysts, such as Cr compounds on silica or other supported IUPAC Periodic Table Group VIB compounds. The catalyst most preferred is a lower valence Group VIB metal oxide on an inert support. Preferred supports include silica, alumina, titania, silica alumina, magnesia and the like. The support material binds the metal oxide catalyst. Those porous substrates having a pore opening of at least  $40 \times 10^{-7}$  mm (40 angstroms) are preferred.

The support material usually has high surface area and large pore volumes with average pore size of  $40$  to  $350 \times 10^{-7}$  mm (40 to 350 angstroms). The high surface area are beneficial for supporting large amount of highly dispersive, active chromium metal centers and to give maximum efficiency of metal usage,

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resulting in very high activity catalyst. The support should have large average pore openings of at least  $40 \times 10^{-7}$  nm (40 angstroms), with an average pore opening of  $>60$  to  $300 \times 10^{-7}$  nm ( $>60$  to 300 angstroms) preferred. This large pore opening will not impose any diffusional restriction of the reactant and product to and away from the active catalytic metal centers, thus further optimizing the catalyst productivity. Also, for this catalyst to be used in fixed bed or slurry reactor and to be recycled and regenerated many times, a silica support with good physical strength is preferred to prevent catalyst particle attrition or disintegration during handling or reaction.

The supported metal oxide catalysts are preferably prepared by impregnating metal salts in water or organic solvents onto the support. Any suitable organic solvent known to the art may be used, for example, ethanol, methanol, or acetic acid. The solid catalyst precursor is then dried and calcined at 200 to  $900^{\circ}\text{C}$  by air or other oxygen-containing gas. Thereafter the catalyst is reduced by any of several various and well known reducing agents such as, for example,  $\text{CO}$ ,  $\text{H}_2$ ,  $\text{NH}_3$ ,  $\text{H}_2\text{S}$ ,  $\text{CS}_2$ ,  $\text{CH}_3\text{SCH}_3$ ,  $\text{CH}_3\text{SSCH}_3$ , metal alkyl containing compounds such as  $\text{R}_3\text{Al}$ ,  $\text{R}_3\text{B}$ ,  $\text{R}_2\text{Mg}$ ,  $\text{RLi}$ ,  $\text{R}_2\text{Zn}$ , where R is alkyl, alkoxy, aryl and the like. Preferred are  $\text{CO}$  or  $\text{H}_2$  or metal alkyl containing compounds. Alternatively, the Group VIB metal may be applied to the substrate in reduced form, such as CrII compounds. The resultant catalyst is very active for oligomerizing olefins at a temperature range from below room temperature to  $250^{\circ}\text{C}$  at a pressure of 10 kPa (0.1 atmosphere) to 34580 kPa (5000 psi). Contact time of both the olefin and the catalyst can vary from one second to 24 hours. The catalyst can be used in a batch type reactor or in a fixed bed, continuous-flow reactor.

In general the support material may be added to a solution of the metal compounds, e.g., acetates or nitrates, etc., and the mixture is then mixed and dried at room



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temperature. The dry solid gel is purged at successively higher temperatures to 600°C for a period of 16 to 20 hours. Thereafter the catalyst is cooled under an inert atmosphere to a temperature of 250 to 450°C and a stream of pure reducing agent is contacted therewith for a sufficiently long period to reduce the catalyst as indicated by a distinct color change from bright orange to pale blue. Typically, the catalyst is treated with an amount of CO equivalent to a two-fold stoichiometric excess to reduce the catalyst to a lower valence CrII state. Finally the catalyst is cooled to room temperature and is ready for use.

The product oligomers have a very wide range of viscosities with high viscosity indices suitable for high performance lubrication use. The product oligomers also have atactic molecular structure of mostly uniform head-to-tail connections with some head-to-head type connections in the structure. These low branch ratio oligomers have high viscosity indices at least 15 to 20 units and typically 30-40 units higher than equivalent viscosity prior art oligomers, which regularly have higher branch ratios and correspondingly lower viscosity indices. These low branch oligomers maintain better or comparable pour points.

The branch ratios, defined as the ratios of CH<sub>3</sub> groups to CH<sub>2</sub> groups in the reaction products and by-products, are calculated from the weight fractions of methyl groups obtained by infrared methods, published in Analytical Chemistry, Vol. 25, No. 10, p. 1466 (1953).

$$\text{Branch ratio} = \frac{\text{wt fraction of methyl group}}{1 - (\text{wt fraction of methyl group})}$$

The unique olefinic dimers used as alkylating agent in the present invention are produced as by-product of the HVI-PAO oligomerization reaction. Typically, in the production of HVI-PAO

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oligomer lubricant base stock, the oligomerization reaction mixture is separated from the catalyst and separated by vacuum distillation to remove unreacted alpha-olefin and lower boiling by-products of the oligomerization reaction, such as alpha-olefin dimer. This provides a lubricant basestock of suitably high volatility and viscosity. While other methods known to those skilled in the art, such as solvent extraction, may be used to separate the alpha-olefin dimer by-product, distillation is preferred.

In the process of the present invention to produce alkylated aromatics, particularly mono-alkylbenzenes, by alkylation with aforementioned dimer, suitable aromatic hydrocarbon starting materials include benzene, mono and di-alkylbenzenes, halobenzenes, alkoxybenzenes, carboxy and carbalkoxy benzenes, phenol, catechol, acetanilide, acetophenone, and the like. Preferred aromatics include benzene, toluene, chlorobenzene and anisole.

The alkylation reaction of the present invention is conducted by contacting a mixture of olefinic dimer and aromatic hydrocarbon with a solid shape selective acidic metallosilicate catalyst having a large pore size. The reaction may be conducted at a temperature between 0 and 300°C, but preferably between 160 and 200°C. The reaction pressure can be between 107 and 7000 kPa (1 psig and 1000 psig), but is preferably 2760 kPa (400 psig). The liquid hourly space velocity (LHSV) based on catalyst can be between .01 and 10, but is preferably between 0.4 and 0.6.

The alkylation reaction can be conducted with or without a solvent. Useful solvents include nitrobenzene, tetrahydrofuran, perchlorobenzene and all such generally higher boiling solvents inert in the alkylation reaction. However, it is preferable to conduct the reaction in the absence of added solvent and more

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preferable to employ an excess of aromatic hydrocarbon reactant as solvent. The process of the present invention can be carried out to produce mono-alkylbenzenes using a mole ratio of reactant benzenes to olefinic dimer alkylating agent of between 50:1 and 0.5:1, preferably between 5:1 and 1:1. The reaction can be carried out in any vessel suitable for the reaction between fluid alkylating agent and benzenes with solid catalyst. Preferably, the reaction is conducted in a fixed bed reactor or a continuous stirred tank reactor but may be effectively carried out in a batch reactor.

Surprisingly, the process of the present invention leads to essentially mono alkylation of aromatic hydrocarbon with olefinic dimer when the alkylation is carried out using acidic shape selective metallocsilicate catalyst such as aluminosilicate zeolite. The shape selective characteristics of zeolite catalysts are well known to those skilled in the art and in the present invention such shape selectivity is deemed to have a determining influence in the surprising limitation of the reaction products to essential monoalkylates. The application of shape-selective catalysis is discussed in "Industrial Application of Shape Selective Catalysis" by N. Y. Chen and W. E. Garwood in Catal. Rev. Sci. Eng., 28(2&3), 185-264 (1986).

Zeolites of interest to shape selective catalysis are divided into three major groups according to their pore/channel systems. These systems include 8-membered oxygen ring systems, 10-membered oxygen ring systems and dual pore systems including 12-membered oxygen ring openings. In general, they are referred to as small, medium or large pore size zeolites proceeding from 8 to 12 membered ring systems. The systems are more completely described in Atlas of Zeolite Structures Types, International Zeolite Assoc., Polycrystal Book Service, Pittsburg, 1978.

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Zeolites useful as catalysts in the present invention include all natural or synthetic acidic large pore size zeolites, typically with a pore size of  $6.4$  to  $7.5 \times 10^{-7}$  mm ( $6.4$  to  $7.5$  Angstroms). Particularly useful catalysts include the acidic form of ZSM-4, ZSM-12, ZSM-20, Faujasite X & Y with pore size of  $7.4 \times 10^{-7}$  mm ( $7.4$  Angstroms) Cancrinite, Gmelinite, Mazzite, Mordenite and Offretite. A preferred catalyst is Faujasite Y.

The following examples are presented to illustrate the present invention and are not intended to limit the scope of the invention.

#### Example 1

##### Catalyst Preparation and Activation Procedure

1.9 grams of chromium (II) acetate ( $\text{Cr}_2(\text{OOCCH}_3)_4 \cdot 2\text{H}_2\text{O}$ ) (5.58 mmole) (commercially obtained) is dissolved in 50 ml of hot acetic acid. Then 50 grams of a silica gel of 8-12 mesh size, a surface area of  $300 \text{ m}^2/\text{g}$ , and a pore volume of 1 ml/g, also is added. Most of the solution is absorbed by the silica gel. The final mixture is mixed for half an hour on a rotavap at room temperature and dried in an open-dish at room temperature. First, the dry solid (20 g) is purged with  $\text{N}_2$  at  $250^\circ\text{C}$  in a tube furnace. The furnace temperature is then raised to  $400^\circ\text{C}$  for 2 hours. The temperature is then set at  $600^\circ\text{C}$  with dry air purging for 16 hours. At this time the catalyst is cooled under  $\text{N}_2$  to a temperature of  $300^\circ\text{C}$ . Then a stream of pure CO (99.99% from Matheson) is introduced for one hour. Finally, the catalyst is cooled to room temperature under  $\text{N}_2$  and ready for use.

#### Example 2

The catalyst prepared in Example 1 (3.2 g) is packed in a 9.5mm (3/8") stainless steel tubular reactor inside an  $\text{N}_2$  blanketed dry box. The reactor under  $\text{N}_2$  atmosphere is then

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heated to 150°C by a single-zone Lindberg furnace. Pre-purified 1-hexene is pumped into the reactor at 1070 kPa (140 psi) and 20 ml/hr. The liquid effluent is collected and stripped of the unreacted starting material and the low boiling material at 5 kPa (0.05 mm Hg). The residual clear, colorless liquid has viscosities and VI's suitable as a lubricant base stock.

Sample	Prerun	1	2	3
T.O.S.*, hr.	2	3.5	5.5	21.5
Lube Yield, wt%	10	41	74	31
Viscosity, mm <sup>2</sup> /s (cS)				
at 40°C	208.5	123.3	104.4	166.2
100°C	26.1	17.1	14.5	20.4
VI	159	151	142	143
*Time on stream				

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Example 3

A commercial chrome/silica catalyst which contains 1% Cr on a large-pore volume synthetic silica gel is used. The catalyst is first calcined with air at 800°C for 16 hours and reduced with CO at 300°C for 1.5 hours. Then 3.5 g of the catalyst is packed into a tubular reactor and heated to 100°C under the N<sub>2</sub> atmosphere. 1-Hexene is pumped through at 28 ml per hour at 101 kPa (1 atmosphere). The products are collected and analyzed as follows:

Sample	C	D	E	F
T.O.S.*, hrs.	3.5	4.5	6.5	22.5
Lube Yield, %	73	64	59	21
Viscosity, mm <sup>2</sup> /s (cS),				
at 40°C	2548	2429	3315	9031
100°C	102	151	197	437
VI	108	164	174	199
*Time on stream				

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Example 4

Five grams of an ammonium Faujasite Y zeolite is placed in a fixed bed reactor. The catalyst is bound with 35% silica. The reactor is heated in air to 538°C and maintained at this temperature for 12 hours. The ammonium Y zeolite is transformed to the hydrogen or acidic Y form. A feed comprised of benzene and by-product C<sub>20</sub> olefinic dimer from the oligomerization of 1-decene in the mole ratio of 5:1 benzene to dimers is passed over the catalyst at 2900 kPa (400 psig). The initial reaction temperature is 160°C at an LHSV of 0.4. At these reaction conditions 88.1% of the dimers are reacted, according to gas chromatographic analysis. After distillation at 220°C and 660 Pa (5mm Hg), the product has the properties presented in Table 1.

Example 5

Using the same feed and catalyst as in Example 5, reaction was carried out at 200°C and 0.6 LHSV. Dimer conversion is 92.8%, according to gas chromatographic analysis. The product properties are presented in Table 1.

Infrared analysis of the mono-alkylbenzenes confirmed that the structures are alkylbenzenes. IR spectra of a model compound, 1-phenyldodecane, when compared to the products made by this method is found to be identical.

Gas chromatographic analysis of the products further shows the presence of C<sub>26</sub> mono-alkyl benzenes. No di-substituted products are noted by GC analysis.

The following elemental analysis and molecular weight determinations are consistent with mono alkyl substitution:

	% Carbon	% Hydrogen	M.W.
Example 5	87.23	13.38	385
Example 6	87.09	12.87	379
Calculated (monoalkyl)	87.15	12.85	358

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Table 1

Example	<u>5</u>	<u>6</u>
Temperature, °C	160	200
Pressure, kPa (psig)	2860 (400)	2860 (400)
5 IHSV	0.4	0.6
% Conversion of Dimer	88.1	92.8
ALKYLATE PROPERTIES		
KV, 40°C	17.80	15.47
KV, 100°C	3.86	3.47
10 Viscosity Index	108.7	99.4
Bromine Number	2.4	4.4
Pour Point, °C	-35.7	-37.5

It has been found that the products of the present invention are useful as additives to mineral oil and synthetic oils when added to those oils in small but sufficient amounts. Lubricants are often formulated with additives to enhance properties for specific applications.

The more commonly used additives include oxidation inhibitors, rust inhibitors, metal passivators, antiwear agents, extreme pressure additives, pour point depressants, detergent-dispersants, viscosity index (VI) improvers, foam inhibitors and the like. This aspect of lubricant arts is specifically described in Kirk-Othmer "Encyclopedia of Chemical Technology", 3rd edition, Vol. 14, pp 477-526. Alkylated aromatics are known in the prior art as lubricant additives for their antiwear properties, thermal and oxidative stability as disclosed in U.S. Patents 4,211,665, 4,238,343, 4,604,491 and 4,714,7944.

Although the present invention has been described with preferred embodiments and examples, it is to be understood that modifications and variations may be resorted to without departing from the spirit and scope of this invention, as those skilled in the art will readily understand. Such modifications and

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variations are considered to be within the purview and scope of the following claims.



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## CLAIMS:

1. A process for the production of mono-alkylbenzenes containing  $C_{16}$ - $C_{28}$  alkyl group from alpha-olefin dimer, comprising;

5 reacting benzene or substituted benzene with  $C_6$ - $C_{14}$  alpha-olefin olefinic dimer having a branch ratio of less than 0.19, or mixture of the dimers, in contact with acidic shape selective metallocsilicate catalyst under alkylating conditions whereby the mono-alkylbenzenes are produced.

2. The process of claim 1 wherein the metallocsilicate catalyst comprises acidic aluminosilicate zeolite-type catalyst containing large pore size.

3. The process of claim 2 wherein the catalyst comprises acidic zeolite containing pore size of  $7.4 \times 10^{-7}$  mm.

4. The process of claim 1 wherein the catalyst comprises acidic X or Y Faujasite.

5. The process of claim 1 wherein the alpha-olefin olefinic dimer comprises the reaction product of the process comprising;

5 contacting  $C_6$ - $C_{14}$  alpha olefin with a supported solid reduced metal oxide catalyst under oligomerization conditions at a temperature of 90 to  $250^{\circ}\text{C}$ , the metal oxide comprising a lower valence form of at least one Group VIB metal to produce lubricant range hydrocarbon product oligomers having a branch ratio of 0.10 to 0.19 and a viscosity index of at least 130;

10 separating the oligomers and recovering the dimer fraction thereof by distillation.

6. The process of claim 5 wherein the supported solid reduced metal oxide catalyst comprises carbon monoxide reduced chromium oxide and the support comprises silica.

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7. The process of claim 5 wherein the alpha-olefins are taken from the group consisting essentially of 1-hexene, 1-octene, 1-decene, 1-dodecene and 1-tetradecene.

8. The process of claim 1 wherein the dimer comprises 1-decene dimer containing 20 carbon atoms.

9. The process of claim 1 wherein the monoalkyl benzenes comprise C<sub>20</sub> alkylbenzenes having a bromine number below 5, viscosity index greater than 90 and pour point below -30°C.

10. The process of claim 1 wherein the alkylating conditions comprise temperature between 0 and 300°C, pressure between 110 and 7000 kPa and liquid hourly space velocity between 0.01 and 10.

11. The process of claim 1 wherein the alkylating conditions comprise temperature between 160 and 200°C, pressure 2860 kPa and liquid hourly space velocity between 0.4 and 0.6.

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# INTERNATIONAL SEARCH REPORT

International Application No PCT/US 90/01714

<b>I. CLASSIFICATION OF SUBJECT MATTER</b> (if several classification symbols apply, indicate all) According to International Patent Classification (IPC) or to both National Classification and IPC IPC <sup>5</sup> : C 07 C 15/107, C 07 C 2/66, C 07 C 2/10														
<b>II. FIELDS SEARCHED</b> <div style="text-align: center; border-top: 1px solid black; border-bottom: 1px solid black;">Minimum Documentation Searched <sup>7</sup></div> <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 30%; border-bottom: 1px solid black;">Classification System</td> <td style="border-bottom: 1px solid black;">Classification Symbols</td> </tr> <tr> <td style="padding: 5px;">IPC<sup>5</sup></td> <td style="padding: 5px;">C 07 C 15/00, C 07 C 2/00</td> </tr> </table> <div style="text-align: center; border-top: 1px solid black; border-bottom: 1px solid black;">Documentation Searched other than Minimum Documentation to the extent that such Documents are included in the Fields Searched <sup>8</sup></div>			Classification System	Classification Symbols	IPC <sup>5</sup>	C 07 C 15/00, C 07 C 2/00								
Classification System	Classification Symbols													
IPC <sup>5</sup>	C 07 C 15/00, C 07 C 2/00													
<b>III. DOCUMENTS CONSIDERED TO BE RELEVANT <sup>9</sup></b> <table style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 10%; border-bottom: 1px solid black;">Category <sup>10</sup></th> <th style="width: 60%; border-bottom: 1px solid black;">Citation of Document, <sup>11</sup> with indication, where appropriate, of the relevant passages <sup>12</sup></th> <th style="width: 30%; border-bottom: 1px solid black;">Relevant to Claim No. <sup>13</sup></th> </tr> <tr> <td style="text-align: center; vertical-align: top; padding: 5px;">A</td> <td style="padding: 5px;">EP, A, 0017457 (MOBIL OIL CORPORATION) 15 October 1980 --</td> <td rowspan="4" style="text-align: center; vertical-align: middle; padding: 5px;">5-7</td> </tr> <tr> <td style="text-align: center; vertical-align: top; padding: 5px;">A</td> <td style="padding: 5px;">US, A, 3631120 (P.E. EBERLY JR. et al.) 28 December 1971 --</td> </tr> <tr> <td style="text-align: center; vertical-align: top; padding: 5px;">P,X</td> <td style="padding: 5px;">US, A, 4827073 (WU) 2 May 1989 see claims; example 22 (cited in the application)  -----</td> </tr> <tr> <td colspan="2" style="height: 100px;"></td> </tr> </table>			Category <sup>10</sup>	Citation of Document, <sup>11</sup> with indication, where appropriate, of the relevant passages <sup>12</sup>	Relevant to Claim No. <sup>13</sup>	A	EP, A, 0017457 (MOBIL OIL CORPORATION) 15 October 1980 --	5-7	A	US, A, 3631120 (P.E. EBERLY JR. et al.) 28 December 1971 --	P,X	US, A, 4827073 (WU) 2 May 1989 see claims; example 22 (cited in the application)  -----		
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<div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> <p><sup>10</sup> Special categories of cited documents: <sup>10</sup></p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 45%;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&amp;" document member of the same patent family</p> </div> </div>														
<b>IV. CERTIFICATION</b> <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; border-bottom: 1px solid black; padding: 5px;">Date of the Actual Completion of the International Search 14th June 1990</td> <td style="width: 50%; border-bottom: 1px solid black; padding: 5px;">Date of Mailing of this International Search Report 16 JUL 1990</td> </tr> <tr> <td style="border-bottom: 1px solid black; padding: 5px;">International Searching Authority EUROPEAN PATENT OFFICE</td> <td style="border-bottom: 1px solid black; padding: 5px;">Signature of Authorized Officer  MISS T. LAZELAAR</td> </tr> </table>			Date of the Actual Completion of the International Search 14th June 1990	Date of Mailing of this International Search Report 16 JUL 1990	International Searching Authority EUROPEAN PATENT OFFICE	Signature of Authorized Officer  MISS T. LAZELAAR								
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**ANNEX TO THE INTERNATIONAL SEARCH REPORT  
ON INTERNATIONAL PATENT APPLICATION NO.**

US 9001714  
SA 36125

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 03/07/90  
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP-A- 0017457	15-10-80	US-A- 4239927	16-12-80
		AU-A- 5695180	09-10-80
		CA-A- 1120062	16-03-82
		JP-A- 55135199	21-10-80
US-A- 3631120	28-12-71	None	
US-A- 4827073	02-05-89	AU-A- 3563289	12-01-90
		WO-A- 8912662	28-12-89
		US-A- 4827064	02-05-89